Title:	RPAD- Resistive Attenuator Design
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Abstract:	This brief memo provides technical back-up to the RPAD computer program.
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1 Introduction

Impedance-matched resistive attenuator design is fundamentally based on the theory of image parameter filters as discussed in §6.2 of [1]. When properly designed, each port of the attenuator provides an ideal impedance match at each respective port.

Given the desired input and output port impedances represented by R_{in} and R_{out} respectively, the minimum attenuator gain that can be realized under the matched condition is given by

$$A_{\min} = \frac{20}{2.3026} \cosh^{-1} \left(\sqrt{\frac{R_{in}}{R_{out}}} \right) \quad \text{dB}$$
(1)

where it has been assumed that $R_{in} \ge R_{out}$.

The design equations for the tee-attenuator shown in Figure 1 are as follows:

$$R_{2} = \frac{\sqrt{R_{in}R_{out}}}{\sinh(A_{np})}$$

$$R_{1} = R_{2} \left[\sqrt{\frac{R_{in}}{R_{out}}} \cosh(A_{np}) - 1 \right]$$

$$R_{3} = R_{2} \left[\sqrt{\frac{R_{out}}{R_{in}}} \cosh(A_{np}) - 1 \right]$$
(2)

and A_{np} is the desired power attenuation factor in units of nepers. Given the desired attenuation A_{dB} in dB,

$$A_{np} = \frac{2.3026}{20} A_{dB}$$
(3)

The design equations for the π -attenuator shown in Figure 2 are similarly given by

$$R_{2} = \sqrt{R_{in}R_{out}} \sinh\left(A_{np}\right)$$

$$R_{1} = R_{2} \left[\sqrt{\frac{R_{out}}{R_{in}}} \cosh\left(A_{np}\right) - 1\right]^{-1}$$

$$R_{3} = R_{2} \left[\sqrt{\frac{R_{in}}{R_{out}}} \cosh\left(A_{np}\right) - 1\right]^{-1}$$
(4)



2 Resultant Characteristics

Since resistors are normally only available in discrete values, it is helpful to compute the resultant attenuator performance once these real-world values have been selected. This can be done in a number of ways by using *z*-, *y*-, or *ABCD*- parameters. The method adopted here is the latter.

The ABCD matrices for the two attenuator types are given by [2]

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\pi} = \begin{bmatrix} 1 & 0 \\ R_{1}^{-1} & 1 \end{bmatrix} \begin{bmatrix} 1 & R_{2} \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ R_{3}^{-1} & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \left(1 + \frac{R_{2}}{R_{3}} \right) & \left(R_{2} \right) \\ \left(R_{1}^{-1} + R_{3}^{-1} + \frac{R_{2}}{R_{1}R_{3}} \right) & \left(1 + \frac{R_{2}}{R_{1}} \right) \end{bmatrix}$$

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{tee} = \begin{bmatrix} 1 & R_{1} \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ R_{2}^{-1} & 1 \end{bmatrix} \begin{bmatrix} 1 & R_{3} \\ 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \left(1 + \frac{R_{1}}{R_{2}} \right) & \left(R_{1} + R_{3} + \frac{R_{1}R_{3}}{R_{2}} \right) \\ R_{2}^{-1} & \left(1 + \frac{R_{3}}{R_{2}} \right) \end{bmatrix}$$
(5)

Given these results, it is a simple matter to compute the corresponding S-parameters from the following relationships:

$$S_{11} = \frac{AR_{out} + B - CR_{in}R_{out} - DR_{in}}{d}$$
(7)

$$S_{12} = \frac{2(AD - BC)\sqrt{R_{in}R_{out}}}{d}$$
(8)

$$S_{21} = \frac{2\sqrt{R_{in}R_{out}}}{d} \tag{9}$$

$$S_{22} = \frac{-AR_{out} + B - CR_{in}R_{out} + DR_{in}}{d}$$
(10)

where

$$d = AR_{out} + B + CR_{in}R_{out} + DR_{in}$$
⁽¹¹⁾

3 Design Example Using RPAD

Assume that a 10 dB Ω -attenuator pad is desired between a source impedance of 50 Ω and a load impedance of 75 Ω . The parameters are entered into the program form as shown in Figure 3 followed by clicking on the *Calculate* button. As also shown, the minimum possible attenuation possible between these two port impedances is 5.72 dB. The user has a choice to select between 1%, 5%, or 10% standard resistor values and all of the nearest-neighbor resistor values permutated as shown. The user is free to select which attenuator design meets their requirements better.

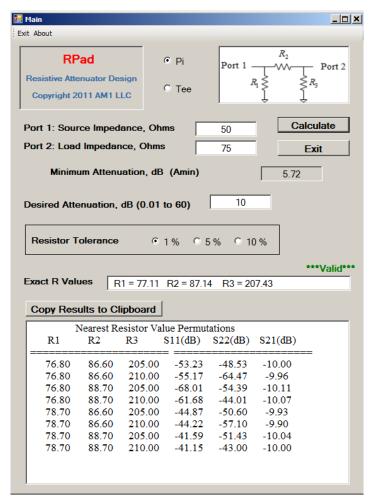


Figure 3 Design example using RPAD

4 References

- 1. Giacoletto, L.J., *Electronics Designers' Handbook*, 2nd ed., McGraw-Hill Book, 1977.
- 2. Davis, W. Alan, *Microwave Semiconductor Circuit Design*, Van Nostrand Reinhold, 1984.